

REVIEW AND SUMMARY FOR CHAPTER 10

Work of a force

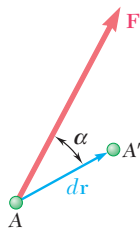


Fig. 10.16

Virtual displacement

Principle of virtual work

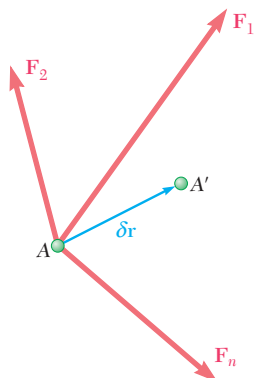


Fig. 10.17

The first part of this chapter was devoted to the *principle of virtual work* and to its direct application to the solution of equilibrium problems. We first defined the *work of a force \mathbf{F} corresponding to the small displacement $d\mathbf{r}$* [Sec. 10.2] as the quantity

$$dU = \mathbf{F} \cdot d\mathbf{r} \quad (10.1)$$

obtained by forming the scalar product of the force \mathbf{F} and the displacement $d\mathbf{r}$ (Fig. 10.16). Denoting respectively by F and ds the magnitudes of the force and of the displacement, and by α the angle formed by \mathbf{F} and $d\mathbf{r}$, we wrote

$$dU = F ds \cos \alpha \quad (10.1')$$

The work dU is positive if $\alpha < 90^\circ$, zero if $\alpha = 90^\circ$, and negative if $\alpha > 90^\circ$. We also found that the *work of a couple of moment \mathbf{M} acting on a rigid body* is

$$dU = M d\theta \quad (10.2)$$

where $d\theta$ is the small angle expressed in radians through which the body rotates.

Considering a particle located at A and acted upon by several forces $\mathbf{F}_1, \mathbf{F}_2, \dots, \mathbf{F}_n$ [Sec. 10.3], we imagined that the particle moved to a new position A' (Fig. 10.17). Since this displacement did not actually take place, it was referred to as a *virtual displacement* and denoted by $\delta\mathbf{r}$, while the corresponding work of the forces was called *virtual work* and denoted by δU . We had

$$\delta U = \mathbf{F}_1 \cdot \delta\mathbf{r} + \mathbf{F}_2 \cdot \delta\mathbf{r} + \dots + \mathbf{F}_n \cdot \delta\mathbf{r}$$

The *principle of virtual work* states that *if a particle is in equilibrium, the total virtual work δU of the forces acting on the particle is zero for any virtual displacement of the particle.*

The principle of virtual work can be extended to the case of rigid bodies and systems of rigid bodies. Since it involves *only forces which do work*, its application provides a useful alternative to the use of the equilibrium equations in the solution of many engineering problems. It is particularly effective in the case of machines and mechanisms consisting of connected rigid bodies, since the work of the reactions at the supports is zero and the work of the internal forces at the pin connections cancels out [Sec. 10.4; Sample Probs. 10.1, 10.2, and 10.3].

In the case of *real machines* [Sec. 10.5], however, the work of the friction forces should be taken into account, with the result that the *output work will be less than the input work*. Defining the *mechanical efficiency* of a machine as the ratio

$$\eta = \frac{\text{output work}}{\text{input work}} \quad (10.9)$$

we also noted that for an ideal machine (no friction) $\eta = 1$, while for a real machine $\eta < 1$.

In the second part of the chapter we considered the *work of forces corresponding to finite displacements* of their points of application. The work $U_{1 \rightarrow 2}$ of the force \mathbf{F} corresponding to a displacement of the particle A from A_1 to A_2 (Fig. 10.18) was obtained by integrating the right-hand member of Eq. (10.1) or (10.1') along the curve described by the particle [Sec. 10.6]:

$$U_{1 \rightarrow 2} = \int_{A_1}^{A_2} \mathbf{F} \cdot d\mathbf{r} \quad (10.11)$$

or

$$U_{1 \rightarrow 2} = \int_{s_1}^{s_2} (F \cos \alpha) ds \quad (10.11')$$

Similarly, the work of a couple of moment \mathbf{M} corresponding to a finite rotation from θ_1 to θ_2 of a rigid body was expressed as

$$U_{1 \rightarrow 2} = \int_{\theta_1}^{\theta_2} M d\theta \quad (10.12)$$

The *work of the weight \mathbf{W} of a body* as its center of gravity moves from the elevation y_1 to y_2 (Fig. 10.19) can be obtained by setting $F = W$ and $\alpha = 180^\circ$ in Eq. (10.11'):

$$U_{1 \rightarrow 2} = - \int_{y_1}^{y_2} W dy = Wy_1 - Wy_2 \quad (10.13)$$

The work of \mathbf{W} is therefore positive *when the elevation y decreases*.

Mechanical efficiency

Work of a force over a finite displacement

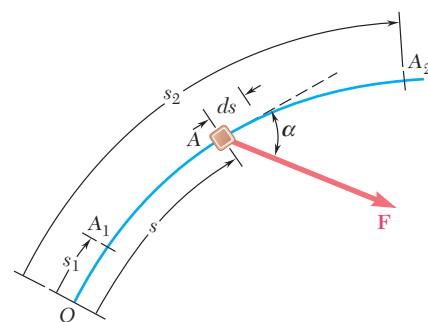


Fig. 10.18

Work of a weight

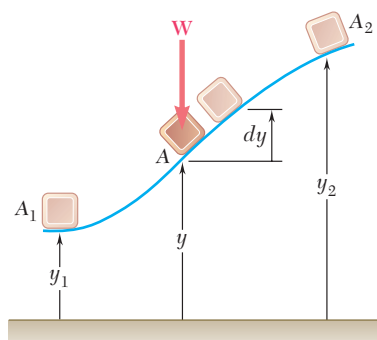


Fig. 10.19

594 Method of Virtual Work

Work of the force exerted by a spring

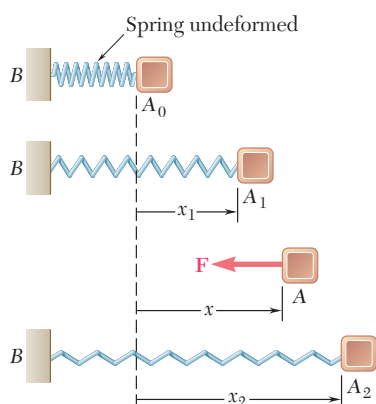


Fig. 10.20

Potential energy

Alternative expression for the principle of virtual work

Stability of equilibrium

The work of the force \mathbf{F} exerted by a spring on a body A as the spring is stretched from x_1 to x_2 (Fig. 10.20) can be obtained by setting $F = kx$, where k is the constant of the spring, and $\alpha = 180^\circ$ in Eq. (10.11')

$$U_{1 \rightarrow 2} = - \int_{x_1}^{x_2} kx \, dx = \frac{1}{2}kx_1^2 - \frac{1}{2}kx_2^2 \quad (10.15)$$

The work of \mathbf{F} is therefore positive when the spring is returning to its undeformed position.

When the work of a force \mathbf{F} is independent of the path actually followed between A_1 and A_2 , the force is said to be a *conservative force*, and its work can be expressed as

$$U_{1 \rightarrow 2} = V_1 - V_2 \quad (10.20)$$

where V is the *potential energy* associated with \mathbf{F} , and V_1 and V_2 represent the values of V at A_1 and A_2 , respectively [Sec. 10.7]. The potential energies associated, respectively, with the *force of gravity* \mathbf{W} and the *elastic force* \mathbf{F} exerted by a spring were found to be

$$V_g = Wy \quad \text{and} \quad V_e = \frac{1}{2}kx^2 \quad (10.17, 10.18)$$

When the position of a mechanical system depends upon a single independent variable θ , the potential energy of the system is a function $V(\theta)$ of that variable, and it follows from Eq. (10.20) that $\delta U = -\delta V = -(dV/d\theta) \delta\theta$. The condition $\delta U = 0$ required by the principle of virtual work for the equilibrium of the system can thus be replaced by the condition

$$\frac{dV}{d\theta} = 0 \quad (10.21)$$

When all the forces involved are conservative, it may be preferable to use Eq. (10.21) rather than to apply the principle of virtual work directly [Sec. 10.8; Sample Prob. 10.4].

This approach presents another advantage, since it is possible to determine from the sign of the second derivative of V whether the equilibrium of the system is *stable*, *unstable*, or *neutral* [Sec. 10.9]. If $d^2V/d\theta^2 > 0$, V is *minimum* and the equilibrium is *stable*; if $d^2V/d\theta^2 < 0$, V is *maximum* and the equilibrium is *unstable*; if $d^2V/d\theta^2 = 0$, it is necessary to examine derivatives of a higher order.