

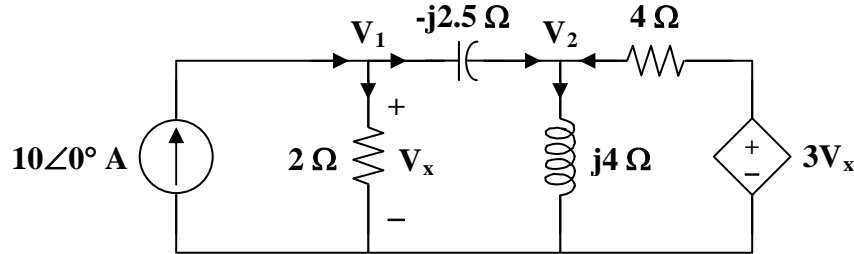
**CHAPTER 10**

**P.P.10.1**  $10\cos(2t) \longrightarrow 10\angle 0^\circ, \omega = 2$

$$2 \text{ H} \longrightarrow j\omega L = j4$$

$$0.2 \text{ F} \longrightarrow \frac{1}{j\omega C} = -j2.5$$

Hence, the circuit in the frequency domain is as shown below.



At node 1,  $10 = \frac{V_1}{2} + \frac{V_1 - V_2}{-j2.5}$

$$100 = (5 + j4)V_1 - j4V_2 \quad (1)$$

At node 2,  $\frac{V_2}{j4} = \frac{V_1 - V_2}{-j2.5} + \frac{3V_x - V_2}{4}$  where  $V_x = V_1$

$$-j2.5V_2 = j4(V_1 - V_2) + 2.5(3V_1 - V_2)$$

$$0 = -(7.5 + j4)V_1 + (2.5 + j1.5)V_2 \quad (2)$$

Put (1) and (2) in matrix form.

$$\begin{bmatrix} 5 + j4 & -j4 \\ -(7.5 + j4) & 2.5 + j1.5 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} 100 \\ 0 \end{bmatrix}$$

where  $\Delta = (5 + j4)(2.5 + j1.5) - (-j4)(-(7.5 + j4)) = 22.5 - j12.5 = 25.74\angle -29.05^\circ$

$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \frac{\begin{bmatrix} 2.5 + j1.5 & j4 \\ 7.5 + j4 & 5 + j4 \end{bmatrix}}{22.5 - j12.5} \begin{bmatrix} 100 \\ 0 \end{bmatrix}$$

$$V_1 = \frac{2.5 + j1.5}{22.5 - j12.5}(100) = \frac{2.915\angle 30.96^\circ}{25.74\angle -29.05^\circ}(100) = 11.325\angle 60.01^\circ \text{ V}$$

$$V_2 = \frac{7.5 + j4}{22.5 - j12.5}(100) = \frac{8.5\angle 28.07^\circ}{25.74\angle -29.05^\circ}(100) = 33.02\angle 57.12^\circ \text{ V}$$

In the time domain,

$$v_1(t) = 11.325\cos(2t + 60.01^\circ) \text{ V}$$

$$v_2(t) = 33.02\cos(2t + 57.12^\circ) \text{ V}$$

**P.P.10.2** The only non-reference node is a supernode.

$$\frac{75 - \mathbf{V}_1}{4} = \frac{\mathbf{V}_1}{j4} + \frac{\mathbf{V}_2}{-j} + \frac{\mathbf{V}_2}{2}$$

$$75 - \mathbf{V}_1 = -j\mathbf{V}_1 + j4\mathbf{V}_2 + 2\mathbf{V}_2$$

$$75 = (1 - j)\mathbf{V}_1 + (2 + j4)\mathbf{V}_2 \quad (1)$$

The supernode gives the constraint of

$$\mathbf{V}_1 = \mathbf{V}_2 + 100\angle 60^\circ \quad (2)$$

Substituting (2) into (1) gives

$$75 = (1 - j)(40\angle 60^\circ) + (3 + j3)\mathbf{V}_2$$

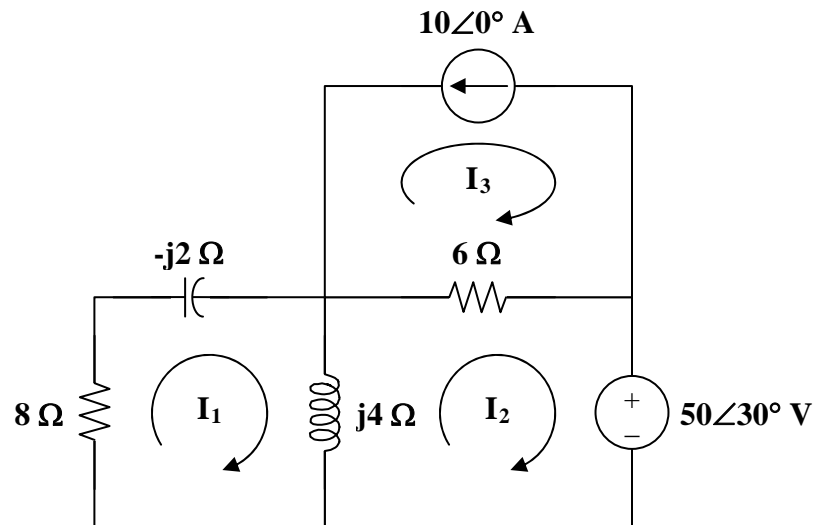
$$\mathbf{V}_2 = \frac{75 - (1 - j)(100\angle 60^\circ)}{3 + j3} = \frac{71.62\angle 210.72^\circ}{4.243\angle 45^\circ} = 16.881\angle 165.72^\circ$$

$$\mathbf{V}_1 = \mathbf{V}_2 + 100\angle 60^\circ = (-16.358 + j4.17) + (50 + j86.6)$$

$$\mathbf{V}_1 = 33.64 + j90.77$$

Therefore,  $\mathbf{V}_1 = 96.8\angle 69.66^\circ \text{ V}$ ,  $\mathbf{V}_2 = 16.88\angle 165.72^\circ \text{ V}$

**P.P.10.3** Consider the circuit below.



For mesh 1,  $(8 - j2 + j4)\mathbf{I}_1 - j4\mathbf{I}_2 = 0$   
 $(8 + j2)\mathbf{I}_1 = j4\mathbf{I}_2 \quad (1)$

For mesh 2,  $(6 + j4)\mathbf{I}_2 - j4\mathbf{I}_1 - 6\mathbf{I}_3 + 50\angle 30^\circ = 0$

For mesh 3,  $\mathbf{I}_3 = -10$

Thus, the equation for mesh 2 becomes

$$(6 + j4)\mathbf{I}_2 - j4\mathbf{I}_1 = -60 - 50\angle 30^\circ \quad (2)$$

From (1),  $\mathbf{I}_2 = \frac{8 + j2}{j4}\mathbf{I}_1 = (0.5 - j2)\mathbf{I}_1$  (3)

Substituting (3) into (2),

$$(6 + j4)(0.5 - j2)\mathbf{I}_1 - j4\mathbf{I}_1 = -60 - 50\angle 30^\circ$$

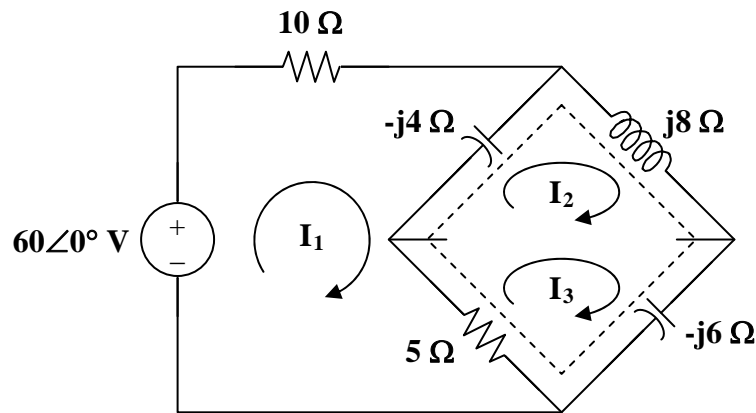
$$(11 - j14)\mathbf{I}_1 = -(103.3 + j25)$$

$$\mathbf{I}_1 = \frac{-(103.3 + j25)}{11 - j14}$$

Hence,  $\mathbf{I}_o = -\mathbf{I}_1 = \frac{103.3 + j25}{11 - j14} = \frac{106.28\angle 13.605^\circ}{17.804\angle -51.843^\circ}$

$$\mathbf{I}_o = 5.969\angle 65.45^\circ \text{ A}$$

**P.P.10.4** Meshes 2 and 3 form a supermesh as shown in the circuit below.



For mesh 1,  $-60 + (15 - j4)\mathbf{I}_1 - (-j4)\mathbf{I}_2 - 5\mathbf{I}_3 = 0$   
 $(15 - j4)\mathbf{I}_1 + j4\mathbf{I}_2 - 5\mathbf{I}_3 = 60$  (1)

For the supermesh,  $(j8 - j4)\mathbf{I}_2 + (5 - j6)\mathbf{I}_3 - (5 - j4)\mathbf{I}_1 = 0$  (2)

Also,  $\mathbf{I}_3 = \mathbf{I}_2 + 2.4$  (3)

Eliminating  $\mathbf{I}_3$  from (1) and (2)

$$(15 - j4)\mathbf{I}_1 + (-5 + j4)\mathbf{I}_2 = 72 \quad (4)$$

$$(-5 + j4)\mathbf{I}_1 + (5 - j2)\mathbf{I}_2 = -12 + j14.4 \quad (5)$$

From (4) and (5),

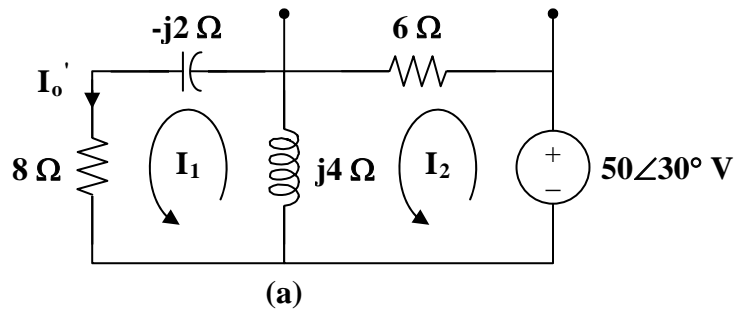
$$\begin{bmatrix} 15 - j4 & -5 + j4 \\ -5 + j4 & 5 - j2 \end{bmatrix} \begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix} = \begin{bmatrix} 72 \\ -12 + j14.4 \end{bmatrix}$$

$$\Delta = \begin{vmatrix} 15 - j4 & -5 + j4 \\ -5 + j4 & 5 - j2 \end{vmatrix} = 58 - j10 = 58.86 \angle -9.78^\circ$$

$$\Delta_1 = \begin{vmatrix} 72 & -5 + j4 \\ -12 + j14.4 & 5 - j2 \end{vmatrix} = 357.6 - j24 = 358.4 \angle -3.84^\circ$$

Thus,  $\mathbf{I}_o = \mathbf{I}_1 = \frac{\Delta_1}{\Delta} = 6.089 \angle 5.94^\circ \text{ A}$

**P.P.10.5** Let  $\mathbf{I}_o = \mathbf{I}'_o + \mathbf{I}''_o$ , where  $\mathbf{I}'_o$  and  $\mathbf{I}''_o$  are due to the voltage source and current source respectively. For  $\mathbf{I}'_o$  consider the circuit in Fig. (a).



For mesh 1,  $(8 + j2)\mathbf{I}_1 - j4\mathbf{I}_2 = 0$   
 $\mathbf{I}_2 = (0.5 - j2)\mathbf{I}_1 \quad (1)$

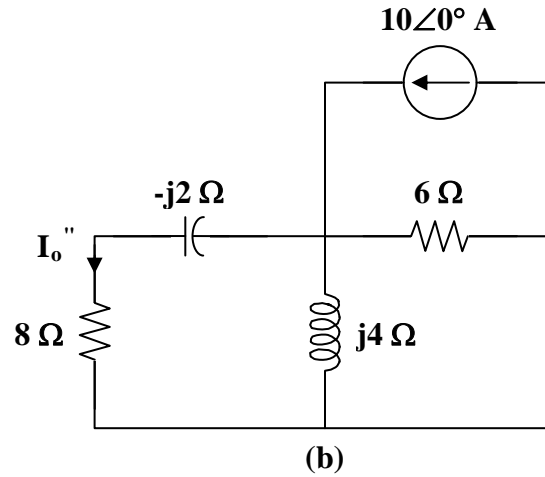
For mesh 2,  $(6 + j4)\mathbf{I}_2 - j4\mathbf{I}_1 - 50 \angle 30^\circ = 0 \quad (2)$

Substituting (1) into (2),

$$(6 + j4)(0.5 - j2)\mathbf{I}_1 - j4\mathbf{I}_1 = 50 \angle 30^\circ$$

$$\mathbf{I}'_o = \mathbf{I}_1 = \frac{50 \angle 30^\circ}{11 - j14} = 0.4 + j2.78$$

For  $\mathbf{I}_o''$  consider the circuit in Fig. (b).



$$\text{Let } \mathbf{Z}_1 = 8 - j2 \Omega, \quad \mathbf{Z}_2 = 6 \parallel j4 = \frac{j24}{6 + j4} = 1.846 + j2.769 \Omega$$

$$\mathbf{I}_o'' = \frac{\mathbf{Z}_2}{\mathbf{Z}_1 + \mathbf{Z}_2} (10) = \frac{(10)(1.846 + j2.769)}{9.846 + j0.77} = 2.082 + j2.65$$

$$\text{Therefore, } \mathbf{I}_o = \mathbf{I}_o' + \mathbf{I}_o'' = 2.48 + j5.43$$

$$\mathbf{I}_o = \mathbf{5.97} \angle \mathbf{65.45}^\circ \text{ A}$$

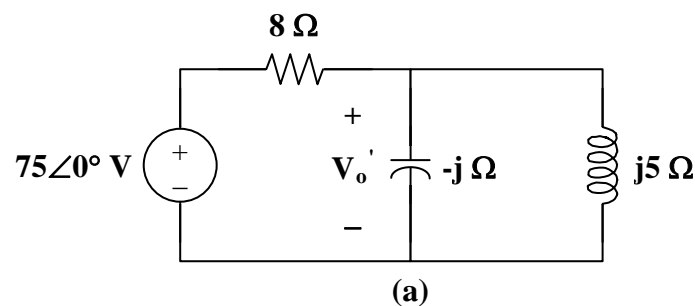
**P.P.10.6** Let  $v_o = v_o' + v_o''$ , where  $v_o'$  is due to the voltage source and  $v_o''$  is due to the current source. For  $v_o'$ , we remove the current source.

$$75 \sin(5t) \longrightarrow 75 \angle 0^\circ, \quad \omega = 5$$

$$0.2 \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(5)(0.2)} = -j$$

$$1 \text{ H} \longrightarrow j\omega L = j(5)(1) = j5$$

The circuit in the frequency domain is shown in Fig. (a).



Note that  $-j \parallel j5 = -j1.25$

By voltage division,

$$\mathbf{V}_o' = \frac{-j1.25}{8 - j1.25}(75) = 11.577 \angle -81.12^\circ$$

Thus,  $v_o' = 11.577 \sin(5t - 81.12^\circ) \text{V}$

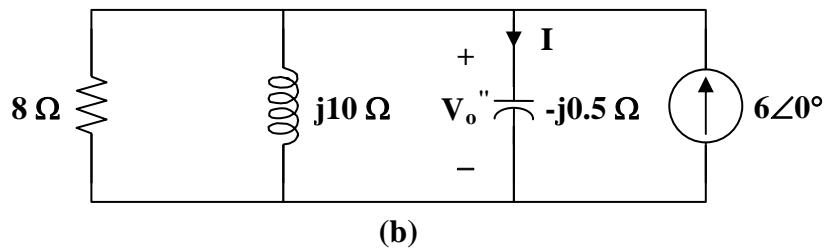
For  $v_o''$ , we remove the voltage source.

$$6 \cos(10t) \longrightarrow 6 \angle 0^\circ, \quad \omega = 10$$

$$0.2 \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(10)(0.2)} = -j0.5$$

$$1 \text{ H} \longrightarrow j\omega L = j(10)(1) = j10$$

The corresponding circuit in the frequency domain is shown in Fig (b).



$$\text{Let } \mathbf{Z}_1 = -j0.5, \quad \mathbf{Z}_2 = 8 \parallel j10 = \frac{j80}{8 + j10} = 4.878 + j3.9$$

By current division,

$$\mathbf{I} = \frac{\mathbf{Z}_2}{\mathbf{Z}_1 + \mathbf{Z}_2}(6)$$

$$\mathbf{V}_o'' = \mathbf{I}(-j0.5) = \frac{\mathbf{Z}_2}{\mathbf{Z}_1 + \mathbf{Z}_2}(6)(-j0.5) = \frac{-j(14.631 + j11.7)}{4.878 + j3.4}$$

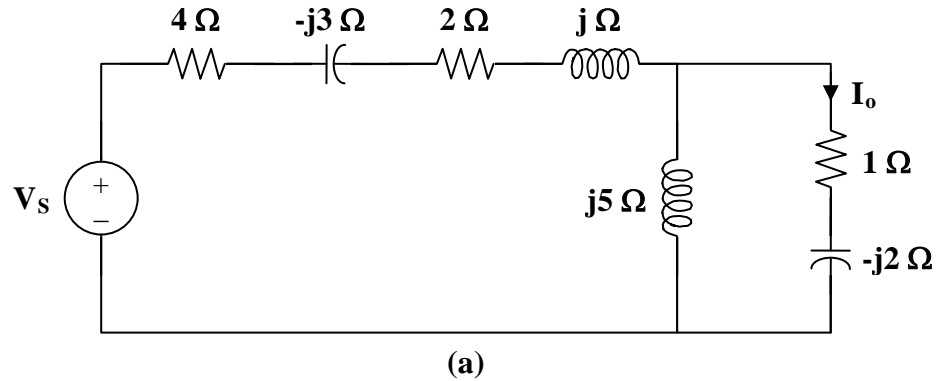
$$\mathbf{V}_o'' = \frac{18.735 \angle -51.36^\circ}{5.94 \angle 34.88^\circ} = 3.154 \angle -86.24^\circ$$

Thus,  $v_o'' = 3.154 \cos(10t - 86.24^\circ)$

Therefore,  $v_o = v_o' + v_o''$

$$v_o = [11.577 \sin(5t - 81.12^\circ) + 3.154 \cos(10t - 86.24^\circ)] \text{ V}$$

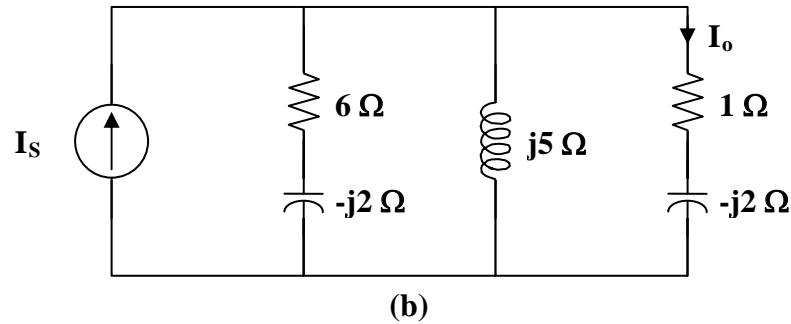
**P.P.10.7** If we transform the current source to a voltage source, we obtain the circuit shown in Fig. (a).



$$\mathbf{V}_s = \mathbf{I}_s \mathbf{Z}_s = (j12)(4 - j3) = 36 + j48$$

We transform the voltage source to a current source as shown in Fig. (b).

Let  $\mathbf{Z} = 4 - j3 + 2 + j = 6 - j2$ . Then,  $\mathbf{I}_s = \frac{\mathbf{V}_s}{\mathbf{Z}} = \frac{36 + j48}{6 - j2} = 4.5 + j9$ .



Note that  $\mathbf{Z} \parallel j5 = \frac{(6 - j2)(j5)}{6 + j3} = \frac{10}{3}(1 + j)$ .

By current division,

$$\mathbf{I}_o = \frac{\frac{10}{3}(1 + j)}{\frac{10}{3}(1 + j) + (1 - j2)}(4.5 + j9)$$

$$\mathbf{I}_o = \frac{-60 + j120}{13 + j4} = \frac{134.16 \angle 116.56^\circ}{13.602 \angle 17.1^\circ}$$

$$\mathbf{I}_o = \mathbf{9.863 \angle 99.46^\circ \text{ A}}$$

**P.P.10.8**

When the voltage source is set equal to zero,

$$\mathbf{Z}_{th} = 10 + (-j4) \parallel (6 + j2)$$

$$\mathbf{Z}_{th} = 10 + \frac{(-j4)(6 + j2)}{6 - j2}$$

$$\mathbf{Z}_{th} = 10 + 2.4 - j3.2$$

$$\mathbf{Z}_{th} = (12.4 - j3.2) \Omega$$

By voltage division,

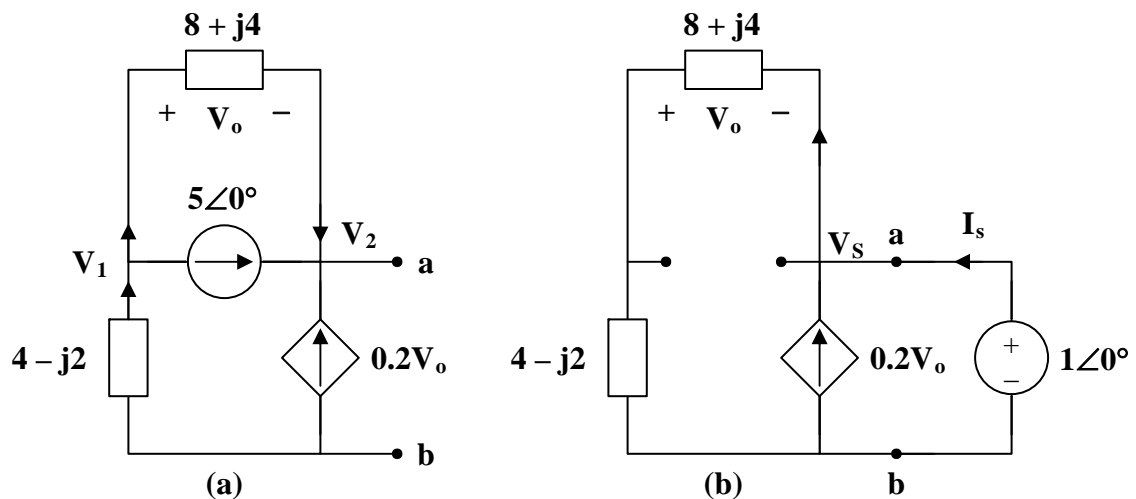
$$\mathbf{V}_{th} = \frac{-j4}{6 + j2 - j4} (100 \angle 20^\circ) = \frac{(-j4)(100 \angle 20^\circ)}{6 - j2}$$

$$\mathbf{V}_{th} = \frac{(4 \angle -90^\circ)(100 \angle 20^\circ)}{6.325 \angle -18.43^\circ}$$

$$\mathbf{V}_{th} = 63.24 \angle -51.57^\circ \text{ V}$$

**P.P.10.9**

To find  $\mathbf{V}_{th}$ , consider the circuit in Fig. (a).



At node 1,

$$\frac{0 - \mathbf{V}_1}{4 - j2} = 5 + \frac{\mathbf{V}_1 - \mathbf{V}_2}{8 + j4}$$

$$-(2 + j)\mathbf{V}_1 = 50 + (1 - j0.5)(\mathbf{V}_1 - \mathbf{V}_2)$$

$$50 = (1 - j0.5)\mathbf{V}_2 - (3 + j0.5)\mathbf{V}_1 \quad (1)$$

At node 2,

$$5 + 0.2\mathbf{V}_o + \frac{\mathbf{V}_1 - \mathbf{V}_2}{8 + j4} = 0,$$

where  $\mathbf{V}_o = \mathbf{V}_1 - \mathbf{V}_2$ .

Hence, the equation for node 2 becomes

$$5 + 0.2(\mathbf{V}_1 - \mathbf{V}_2) + \frac{\mathbf{V}_1 - \mathbf{V}_2}{8 + j4} = 0$$



$$\mathbf{V}_1 = \mathbf{V}_2 - \frac{50}{3 + j0.5} \quad (2)$$

Substituting (2) into (1),

$$50 = (1 - j0.5)\mathbf{V}_2 - (3 + j0.5)\mathbf{V}_2 + (50) \frac{3 + j0.5}{3 - j0.5}$$

$$0 = -50 - (2 + j)\mathbf{V}_2 + \frac{50}{37}(35 + j12)$$

$$\mathbf{V}_2 = \frac{-2.702 + j16.22}{2 + j} = 7.35 \angle 72.9^\circ$$

$$\mathbf{V}_{th} = \mathbf{V}_2 = \mathbf{7.35} \angle \mathbf{72.9^\circ} \mathbf{V}$$

To find  $\mathbf{Z}_{th}$ , we remove the independent source and insert a 1-V voltage source between terminals a-b, as shown in Fig. (b).

At node a, 
$$\mathbf{I}_s = -0.2\mathbf{V}_o + \frac{\mathbf{V}_s}{8 + j4 + 4 - j2}$$

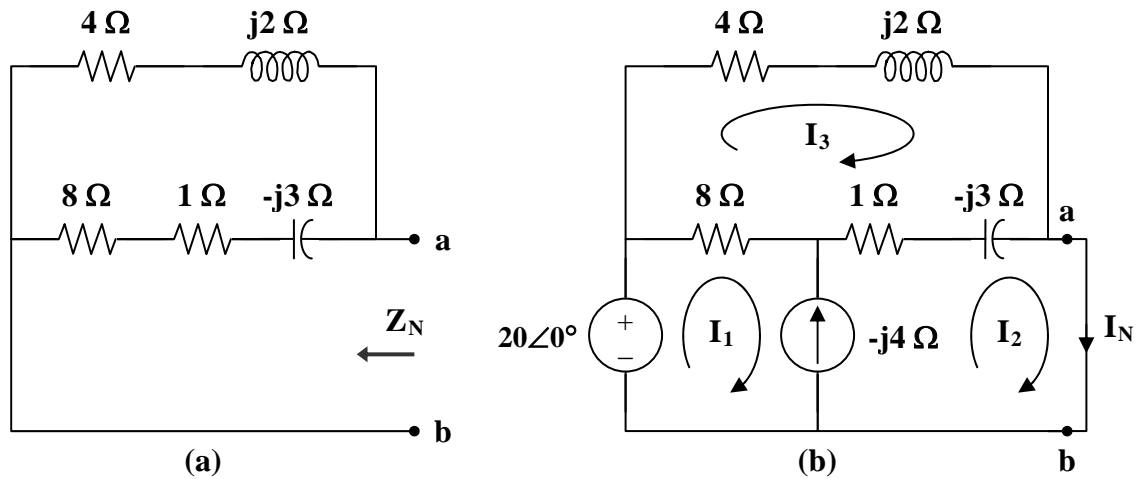
But, 
$$\mathbf{V}_s = 1 \quad \text{and} \quad -\mathbf{V}_o = \frac{8 + j4}{8 + j4 + 4 - j2} \mathbf{V}_s$$

So, 
$$\mathbf{I}_s = (0.2) \frac{8 + j4}{12 + j2} + \frac{1}{12 + j2} = \frac{2.6 + j0.8}{12 + j2}$$

and 
$$\mathbf{Z}_{th} = \frac{\mathbf{V}_s}{\mathbf{I}_s} = \frac{1}{\mathbf{I}_s} = \frac{12 + j2}{2.6 + j0.8} = \frac{12.166 \angle 9.46^\circ}{2.72 \angle 17.10^\circ}$$

$$\mathbf{Z}_{th} = \mathbf{4.473} \angle \mathbf{-7.64^\circ} \mathbf{\Omega}$$

**P.P.10.10** To find  $Z_N$ , consider the circuit in Fig. (a).



$$Z_N = (4 + j2) \parallel (9 - j3) = \frac{(4 + j2)(9 - j3)}{13 - j}$$

$$Z_N = (3.176 + j0.706) \Omega$$

To find  $I_N$ , short-circuit terminals a-b as shown in Fig. (b). Notice that meshes 1 and 2 form a supermesh.

$$\text{For the supermesh, } -20 + 8I_1 + (1 - j3)I_2 - (9 - j3)I_3 = 0 \quad (1)$$

$$\text{Also, } I_1 = I_2 + j4 \quad (2)$$

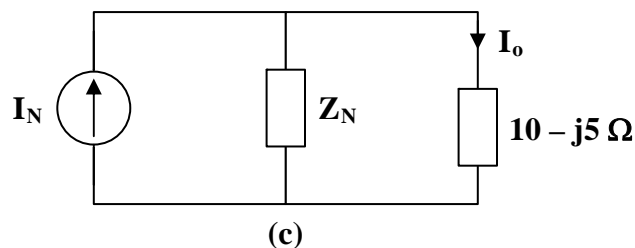
$$\text{For mesh 3, } (13 - j)I_3 - 8I_1 - (1 - j3)I_2 = 0 \quad (3)$$

Solving for  $I_2$ , we obtain

$$I_N = I_2 = \frac{50 - j62}{9 - j3} = \frac{79.65 \angle -51.11^\circ}{9.487 \angle -18.43^\circ}$$

$$I_N = 8.396 \angle -32.68^\circ \text{ A}$$

Using the Norton equivalent, we can find  $I_o$  as in Fig. (c).



By current division,

$$\mathbf{I}_o = \frac{\mathbf{Z}_N}{\mathbf{Z}_N + 10 - j5} \mathbf{I}_N = \frac{3.176 + j0.706}{13.176 - j4.294} (8.396 \angle -32.68^\circ)$$

$$\mathbf{I}_o = \frac{(3.254 \angle 12.53^\circ)(8.396 \angle -32.68^\circ)}{13.858 \angle -18.05^\circ}$$

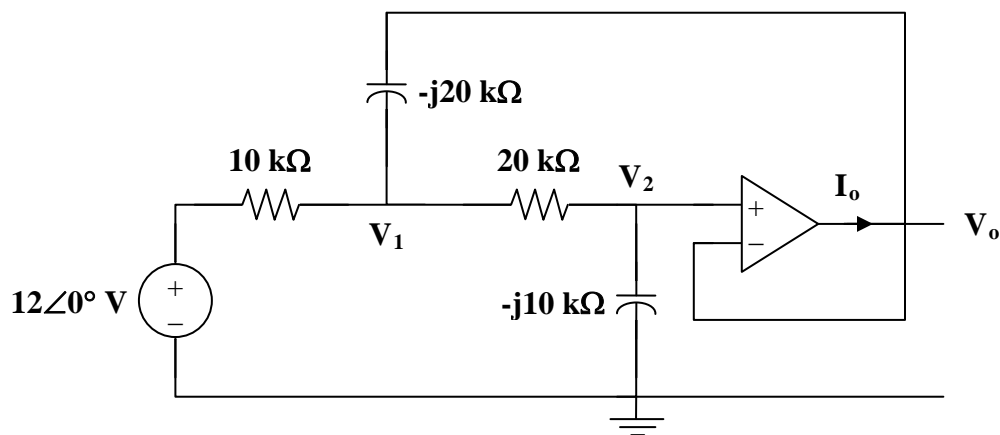
$$\mathbf{I}_o = 1.9714 \angle -2.10^\circ \text{ A}$$

**P.P.10.11**

$$10 \text{ nF} \longrightarrow \frac{1}{j\omega C_1} = \frac{1}{j(5 \times 10^3)(10 \times 10^{-9})} = -j20 \text{ k}\Omega$$

$$20 \text{ nF} \longrightarrow \frac{1}{j\omega C_2} = \frac{1}{j(5 \times 10^3)(20 \times 10^{-9})} = -j10 \text{ k}\Omega$$

Consider the circuit in the frequency domain as shown below.



As a voltage follower,  $\mathbf{V}_2 = \mathbf{V}_o$

At node 1,

$$\frac{12 - \mathbf{V}_1}{10} = \frac{\mathbf{V}_1 - \mathbf{V}_o}{-j20} + \frac{\mathbf{V}_1 - \mathbf{V}_o}{20}$$

$$24 = (3 + j)\mathbf{V}_1 - (1 + j)\mathbf{V}_o \quad (1)$$

At node 2,

$$\frac{\mathbf{V}_1 - \mathbf{V}_o}{20} = \frac{\mathbf{V}_o - 0}{-j10}$$

$$\mathbf{V}_1 = (1 + j2)\mathbf{V}_o \quad (2)$$

Substituting (2) into (1) gives

$$24 = j6\mathbf{V}_o \quad \text{or} \quad \mathbf{V}_o = 4 \angle -90^\circ$$

Hence,  $v_o(t) = 4\cos(5000t - 90^\circ) V$   
 $v_o(t) = \mathbf{4\sin(5,000t) V}$

Now,  $I_o = \frac{V_o - V_1}{-j20k}$

But from (2)  $V_o - V_1 = -j2V_o = -8$

$$I_o = \frac{-8}{-j20k} = -j400 \mu A$$

Hence,  $i_o(t) = 400\cos(5000t - 90^\circ) \mu A$

$$i_o(t) = \mathbf{400\sin(5,000t) \mu A}$$

**P.P.10.12** Let  $Z = R \parallel \frac{1}{j\omega C} = \frac{R}{1 + j\omega RC}$

$$\frac{V_s}{V_o} = \frac{R}{R + Z}$$

The loop gain is

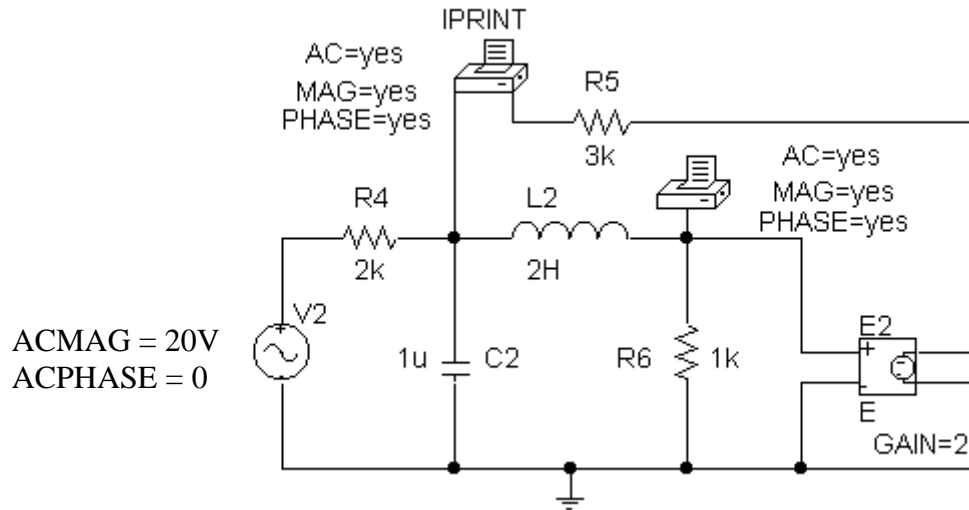
$$1/G = \frac{V_s}{V_o} = \frac{R}{R + Z} = \frac{R}{R + \frac{R}{1 + j\omega RC}} = \frac{1 + j\omega RC}{2 + j\omega RC}$$

where  $\omega RC = (1000)(10 \times 10^3)(1 \times 10^{-6}) = 10$

$$1/G = \frac{1 + j10}{2 + j10} = \frac{10.05 \angle 84.29^\circ}{10.2 \angle 78.69^\circ}$$

$$G = \mathbf{1.0147 \angle -5.6^\circ}$$

**P.P.10.13** The schematic is shown below.



Since  $\omega = 2\pi f = 3000 \text{ rad/s} \longrightarrow f = 477.465 \text{ Hz}$ . Setup/Analysis/AC Sweep as Linear for 1 point starting and ending at a frequency of 447.465 Hz. When the schematic is saved and run, the output file includes

Frequency	IM(V_PRINT1)	IP(V_PRINT1)
4.775E+02	1.088E-03	-5.512E+01
Frequency	VM(\$N_0005)	VP(\$N_0005)
4.775E+02	5.364E-01	-1.546E+02

From the output file, we obtain

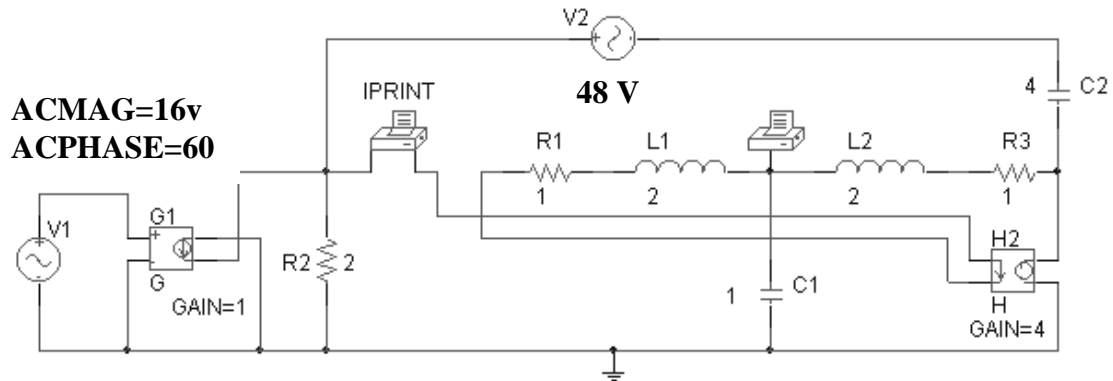
$$\mathbf{V}_o = 0.2682 \angle -154.6^\circ \text{ V} \quad \text{and} \quad \mathbf{I}_o = 0.544 \angle -55.12^\circ \text{ mA}$$

Therefore,

$$v_o(t) = 536.4 \cos(3,000t - 154.6^\circ) \text{ mV}$$

$$i_o(t) = 1.088 \cos(3,000t - 55.12^\circ) \text{ mA}$$

**P.P.10.14** The schematic is shown below.



Since PSpice does not allow the use of complex impedances, we need to convert the complex impedances into values of capacitance and inductance. We select  $\omega = 1$  rad/s which generates  $f = 0.15915$  Hz. We use this to obtain the values of capacitances, where  $C = 1/\omega X_c$ , and inductances, where  $L = X_L/\omega$ . Since AC current sources in PSpice does not allow the use of phase angles but AC voltages do, we can replace the current source with a voltage controlled current source. Thus we not have created an AC current source with a magnitude and a phase.

To obtain the desired output use Setup/Analysis/AC Sweep as Linear for 1 point starting and ending at a frequency of 0.15915 Hz. When the schematic is saved and run, the output file includes

Frequency	IM(V_PRINT1)	IP(V_PRINT1)
1.592E-01	10.336E+00	1.580E+02
Frequency	VM(\$N_0004)	VP(\$N_0004)
1.592E-01	39.368E+00	4.478E+01

From the output file, we obtain

$$\mathbf{V_x = 39.37 \angle 44.78^\circ \text{ V} \quad \text{and} \quad \mathbf{I_x = 10.336 \angle 158^\circ \text{ A}}$$

**P.P.10.15** 
$$C_{eq} = \left(1 + \frac{R_2}{R_1}\right) C = \left(1 + \frac{10 \times 10^6}{10 \times 10^3}\right) (10 \times 10^{-9}) = \mathbf{10 \mu F}$$

**P.P.10.16** If  $R = R_1 = R_2 = 2.5 \text{ k}\Omega$  and  $C = C_1 = C_2 = 1 \text{ nF}$

$$f_o = \frac{1}{2\pi RC} = \frac{1}{(2\pi)(2.5 \times 10^3)(1 \times 10^{-9})} = \mathbf{63.66 \text{ kHz}}$$